

The eye of sauron

THE POTENTIAL ENERGY OF RESIDUALLY STRESSED SOLIDS

Author:
Artur L. Gower

Co-Author:
Dr. Pasquale Ciarletta

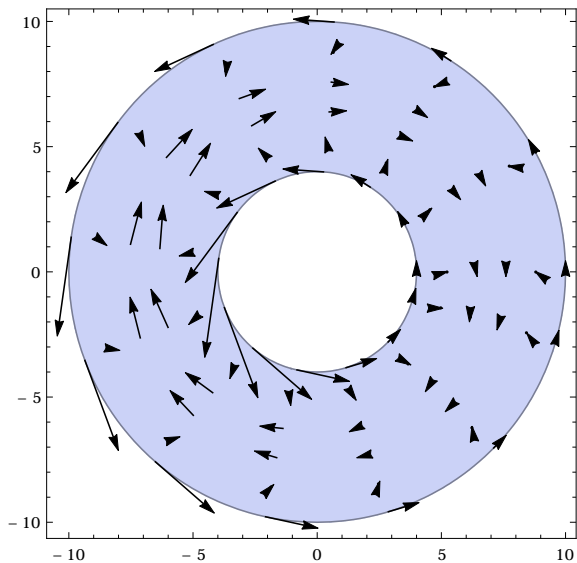
Supervisor:
prof. Michel Destrade

National University of Ireland Galway

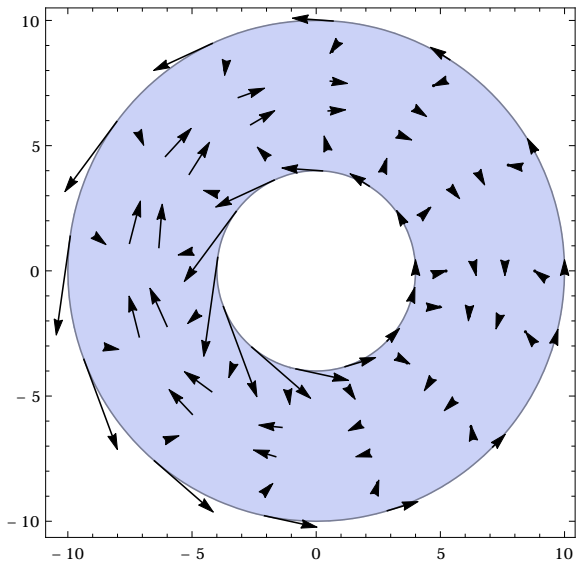


NUI Galway
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Measurement from hell



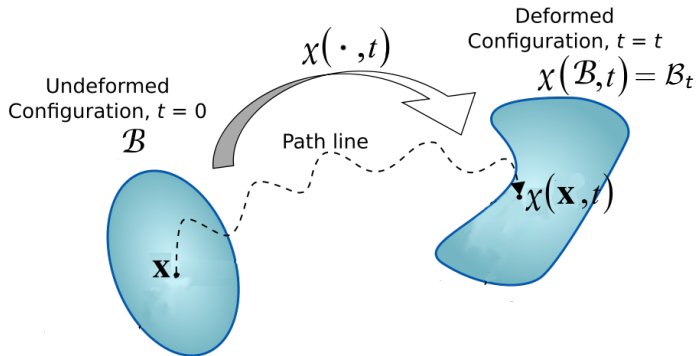
Measurement from hell



How do we deal with this? Energy $W(\mathbf{B}, \tau)$

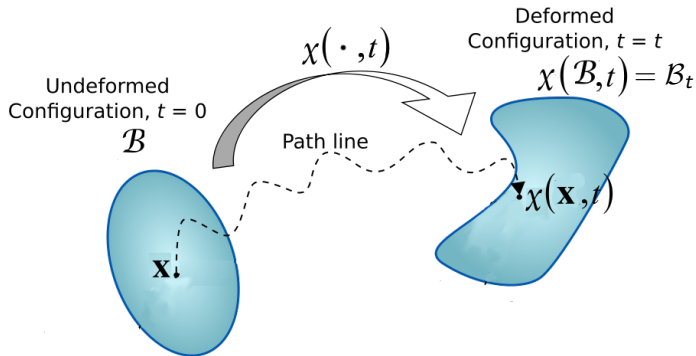
Continuum Blob Mechanics

We apply the laws of physics to a continuous blob which is moving through space.



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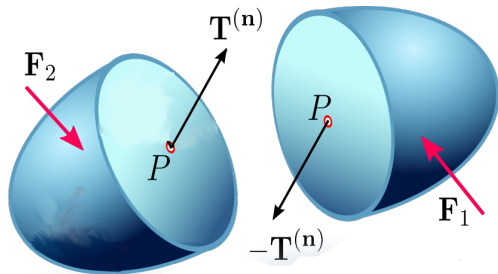
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With each position $x = \chi(X, t)$ we associate densities such as mass $\rho(x, t)$ and stress $\mathbf{T}^{(n)}(x, t)$.

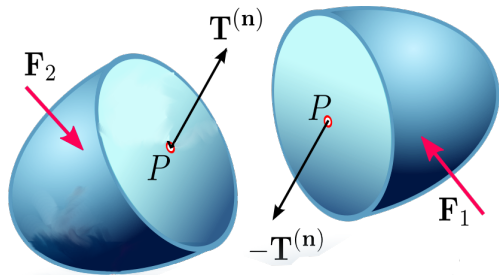
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To describe the forces $\mathbf{F}_1(\mathbf{X}, t)$, $\mathbf{F}_2(\mathbf{X}, t)$, $\mathbf{T}^{(n)}(\mathbf{X}, t)$, $\mathbf{n} \in T_x\mathcal{B}_t$, we make an imaginary slice



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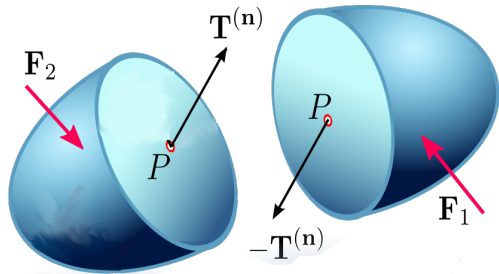
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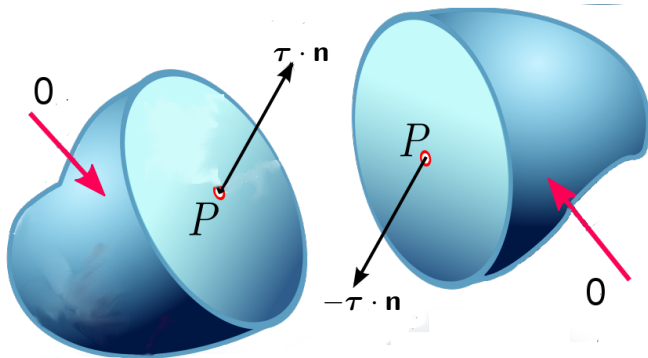


The forces \mathbf{F}_1 and \mathbf{F}_2 may be determined by Boundary conditions. While the internal stress $\mathbf{T}^{(n)}$ can be written as $\mathbf{T}^{(n)} = \boldsymbol{\sigma} \cdot \mathbf{n}$.
(One of Cauchy's many theories).

■ We call $\boldsymbol{\sigma}$ a stress tensor, with $\boldsymbol{\sigma}(X, t) \in T_x\mathcal{B}_t \otimes T_x\mathcal{B}_t$.

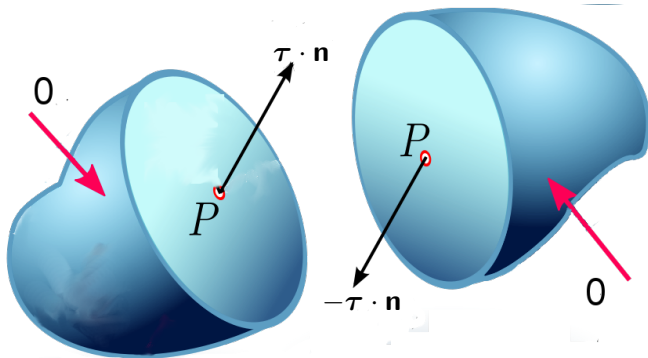
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The residual stress tensor $\tau = \sigma$, when all external load is removed.



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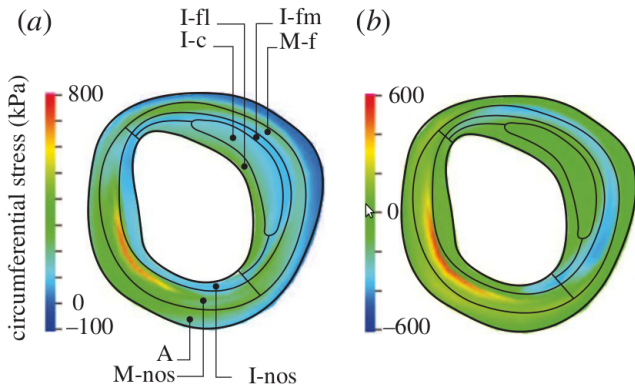
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To incorporate the residual stress τ into the mechanics, we use the above as a reference state.

Continuum Blob Mechanics

The circumferential stress in the cross section of an artery:



(a) is unloaded, (b) is loaded (assuming isotropy).

Assumptions of Elasticity

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The result $W(X, t) = \hat{W}(\mathbf{C}(X, t), \boldsymbol{\tau}(X))$, where $\mathbf{C}(X, t) = \mathbf{D}\chi^T(X, t)\mathbf{D}\chi(X, t)$ and

$$\boldsymbol{\sigma}(X, t) = 2\rho\mathbf{D}\chi(X, t)\frac{\partial\hat{W}}{\partial\mathbf{C}}(\mathbf{C}(X, t), \boldsymbol{\tau}(X))\mathbf{D}\chi^T(X, t).$$

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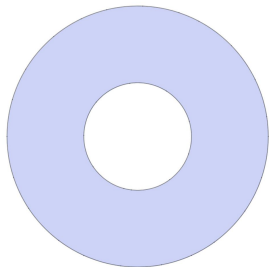
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- What remains is to specify the dependance of \hat{W} on \mathbf{C} and $\boldsymbol{\tau}$...

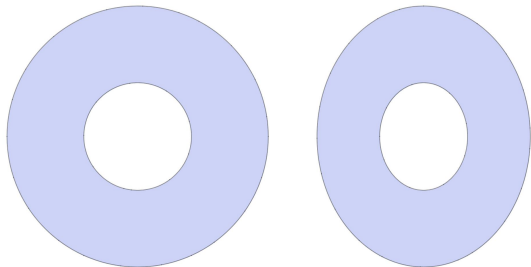
Squeezing a Donut

Without the residual stress τ we know that



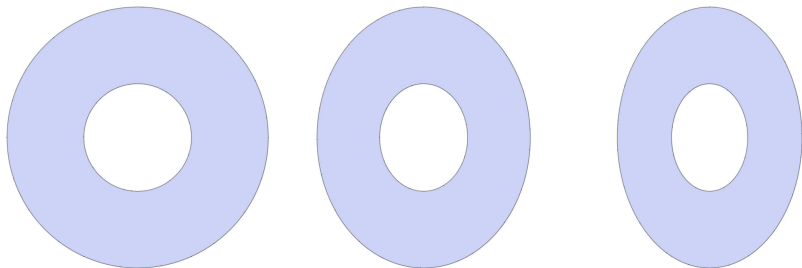
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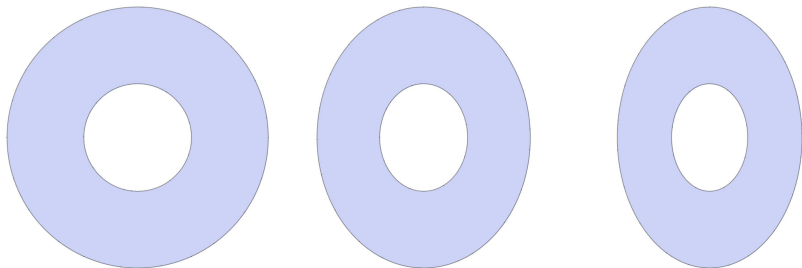
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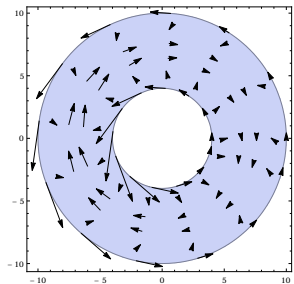
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→ Potential energy $\hat{W}(\mathbf{C}, \mathbf{0})$ increases →

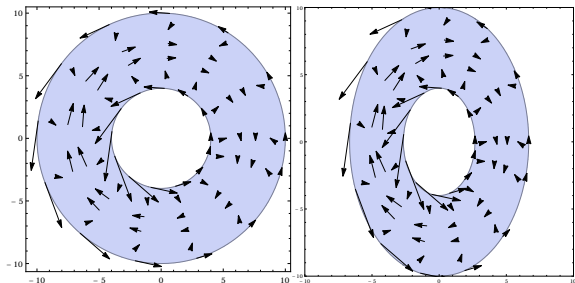
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For a residually stressed body it is not so clear



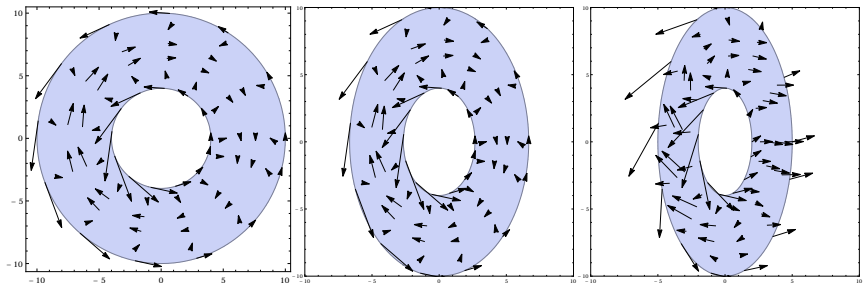
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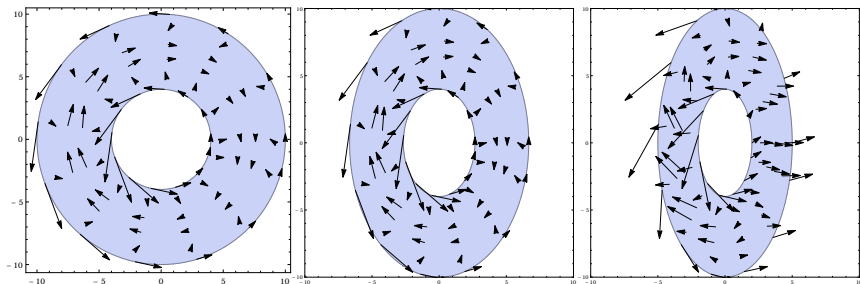
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→ how does the potential energy $\hat{W}(\mathbf{C}, \boldsymbol{\tau})$ change? →

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Independent of a rotation of the reference configuration:

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$$\hat{W}(\mathbf{C}, \mathbf{0}) = \hat{W} \left(\begin{pmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{pmatrix}, \mathbf{0} \right) = \Psi(\text{tr } \mathbf{C}, (\text{tr } \mathbf{C})^2 - \text{tr } \mathbf{C}^2, \det \mathbf{C}).$$

where

$$\begin{aligned} \text{tr } \mathbf{C} &= \lambda_1 + \lambda_2 + \lambda_3, \\ (\text{tr } \mathbf{C})^2 - \text{tr } \mathbf{C}^2 &= \lambda_1 \lambda_2 + \lambda_2 \lambda_3 + \lambda_3 \lambda_1 - 3 \\ \det \mathbf{C} &= \lambda_1 \lambda_2 \lambda_3. \end{aligned}$$

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One successful expansion

$$\hat{W}(\mathbf{C}, \mathbf{0}) = C_1 \text{tr } \mathbf{C} + C_2 ((\text{tr } \mathbf{C})^2 - \text{tr } \mathbf{C}^2) + C_3 \det \mathbf{C}.$$

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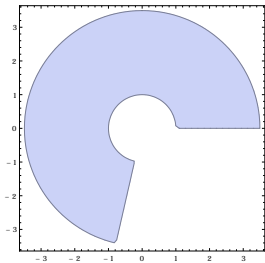
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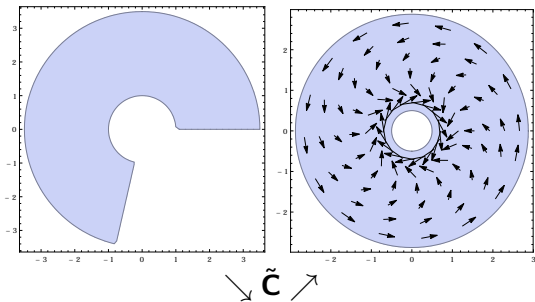
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What expansion to use?

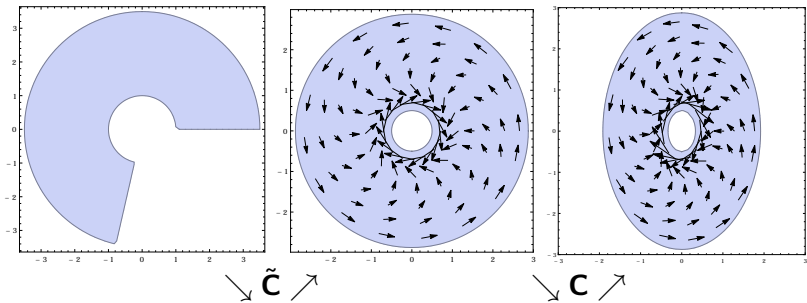
A Geometric Fix



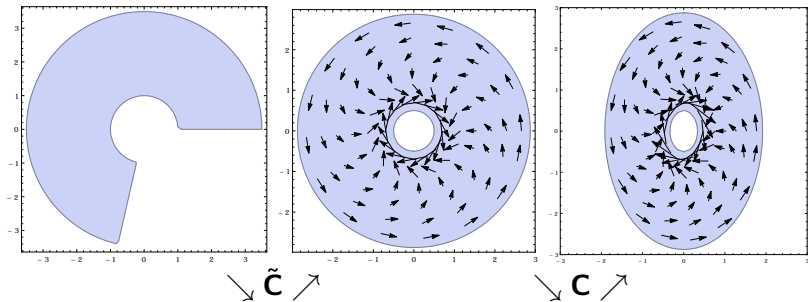
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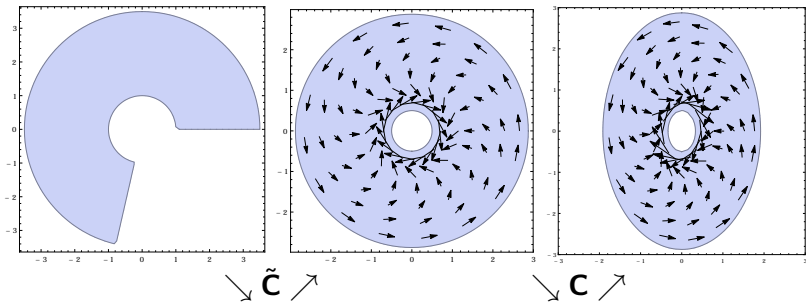
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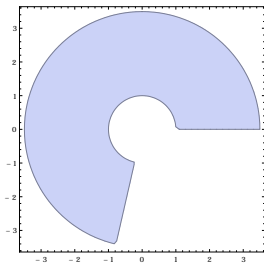
↓ Cut and check.



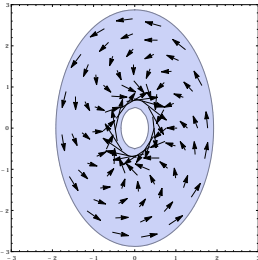
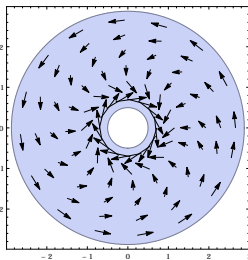
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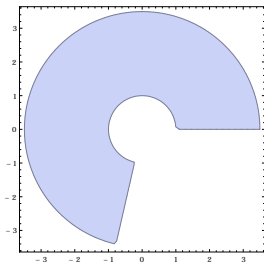
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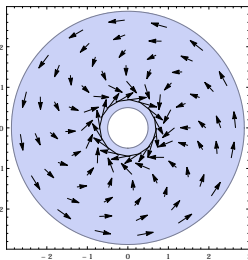
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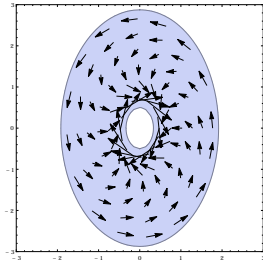
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↓ Guess W_C



↓ Fit Data.

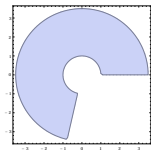


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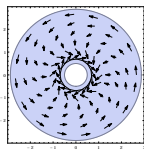
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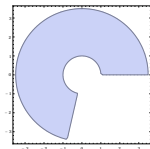
A Geometric Fix



$$\xrightarrow{\tilde{\chi}(R, \theta)}$$

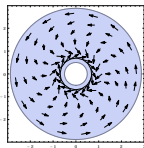


A Geometric Fix

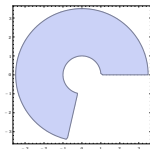


$$A \leq R \leq B$$
$$0 \leq \theta \leq \theta_0$$

$$\xrightarrow{\tilde{\chi}(R, \theta)}$$

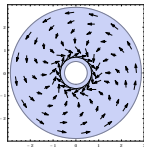


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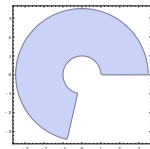


$$A \leq R \leq B$$
$$0 \leq \Theta \leq \Theta_0$$

$$\xrightarrow{\tilde{\chi}(R, \Theta)}$$
$$\parallel$$
$$(r(R), \Theta(\theta))$$



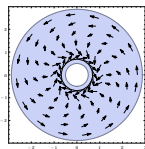
A Geometric Fix



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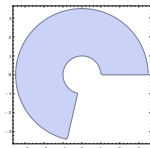
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$$a \leq r(R) \leq b$$
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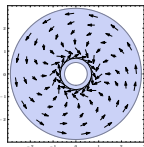
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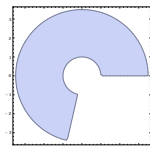


$$a \leq r(R) \leq b$$
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Incompressibility means

$$\det \mathbf{D}\tilde{\chi} = 1 \implies \det \begin{pmatrix} r_R & 0 \\ 0 & \theta_\Theta \end{pmatrix} = 1$$

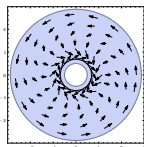
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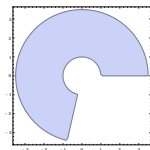


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$$\det \mathbf{D}\tilde{\chi} = 1 \implies \det \begin{pmatrix} r_R & 0 \\ 0 & \theta_\Theta \end{pmatrix} = 1 \implies r_R \theta_\Theta / R = 1$$

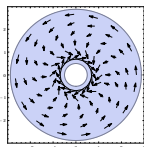
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Incompressibility means

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$$\implies \theta(\Theta) = \frac{2\pi}{\Theta_0} \Theta \text{ and } r(R) = \sqrt{a^2 + \frac{\Theta_0}{2\pi} (R^2 - A^2)}$$

A Geometric Fix

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implying that

$$\boldsymbol{\tau} = \begin{pmatrix} \tau_{rr} & 0 \\ 0 & \tau_{\theta\theta} \end{pmatrix} = \begin{pmatrix} r_R^2(R) - p(R) & 0 \\ 0 & \theta_\Theta^2(\Theta)/R^2 - p(R) \end{pmatrix},$$

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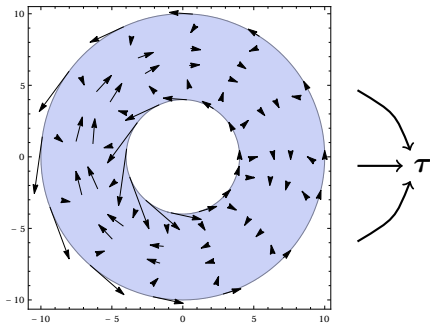
$$\tau_{rr}(A) = r_R^2(A) - p(A) = 0 = \tau_{rr}(B) = r_R^2(B) - p(B).$$

Plug into equilibrium equation

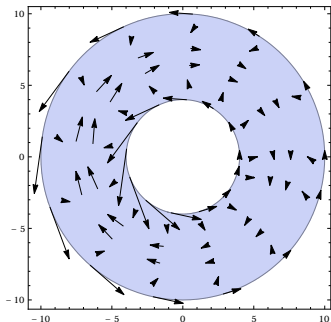
$$\text{div } \boldsymbol{\tau} = 0 \implies r/r_R \partial_R \tau_{rr} + \tau_{rr} - \tau_{\theta\theta} = 0,$$

solve for $p(R)$.

Stress τ as Input

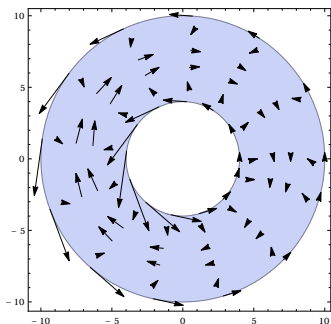


Stress τ as Input



$$\tau \longrightarrow \tilde{\mathbf{B}}(\tau) = \mathbf{D}_\chi \mathbf{D}_\chi^T$$

Stress τ as Input



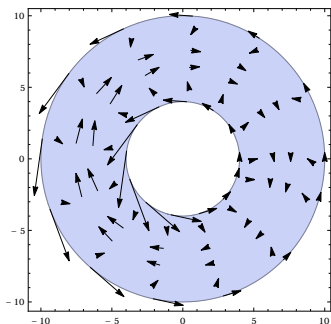
$$\tau \longrightarrow \tilde{\mathbf{B}}(\tau) = \mathbf{D}\chi\mathbf{D}\chi^T$$

Adopting

$$W(\mathbf{C}, \tau) = W_C(\tilde{\mathbf{C}}\mathbf{C}) = \frac{\mu}{2} \left(\text{tr}(\tilde{\mathbf{C}}\mathbf{C}) - 3 \right) = \frac{\mu}{2} \left(\text{tr}(\mathbf{B}\tilde{\mathbf{B}}(\tau)) - 3 \right).$$

(remember $\mathbf{C} = \mathbf{D}\chi^T\mathbf{D}\chi$).

Stress τ as Input



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(remember $\mathbf{C} = \mathbf{D}\chi^T\mathbf{D}\chi$).

- Though we assume there is a virtual stress-free state, that gives $\tilde{\mathbf{C}}$, we don't know what it looks like!

Stress $\boldsymbol{\tau}$ as Input

To find $\tilde{\mathbf{B}}(\boldsymbol{\tau})$:

$$\boldsymbol{\tau} = \mu\rho\mathbf{D}\tilde{\boldsymbol{\chi}}\frac{\partial\text{tr}\tilde{\mathbf{C}}}{\partial\tilde{\mathbf{C}}}\mathbf{D}\tilde{\boldsymbol{\chi}}^T - p\mathbf{I} = \mu\tilde{\mathbf{B}} - p\mathbf{I},$$

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Assume $\tilde{\mathbf{B}}$ incompressible, then after some algebra an inversion is possible.

Stress $\boldsymbol{\tau}$ as Input

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Assume $\tilde{\mathbf{B}}$ incompressible, then after some algebra an inversion is possible. Plain strain example:

$$\tilde{\mathbf{B}} = \frac{1}{\mu} \boldsymbol{\tau} + \frac{1}{2\mu} \left(-\text{tr } \boldsymbol{\tau} + \sqrt{4\mu^2 + (\text{tr } \boldsymbol{\tau})^2 - 4 \det \boldsymbol{\tau}} \right) \mathbf{I},$$

Stress $\boldsymbol{\tau}$ as Input

To find $\tilde{\mathbf{B}}(\boldsymbol{\tau})$:

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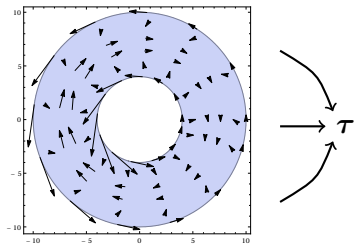
$$\tilde{\mathbf{B}} = \frac{1}{\mu}\boldsymbol{\tau} + \frac{1}{2\mu} \left(-\text{tr } \boldsymbol{\tau} + \sqrt{4\mu^2 + (\text{tr } \boldsymbol{\tau})^2 - 4 \det \boldsymbol{\tau}} \right) \mathbf{I},$$

then using $W(\mathbf{C}, \boldsymbol{\tau}) = W_C(\mathbf{B}\tilde{\mathbf{B}})$, leading to

$$W(\mathbf{C}, \boldsymbol{\tau}) = \frac{1}{2}\text{tr}(\mathbf{B}\boldsymbol{\tau}) + \frac{1}{4}\text{tr}\mathbf{B} \left(-\text{tr}\boldsymbol{\tau} + \sqrt{4\mu^2 + (\text{tr } \boldsymbol{\tau})^2 - 4 \det \boldsymbol{\tau}} \right) - \mu$$

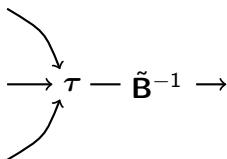
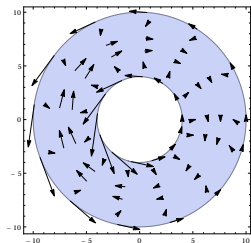
Stress τ as Input

Looking for a "cut" stress-free state:



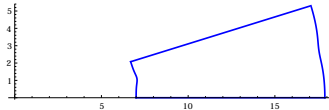
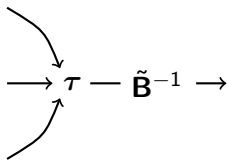
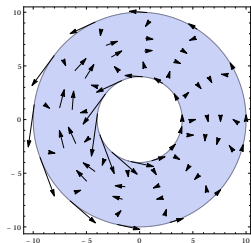
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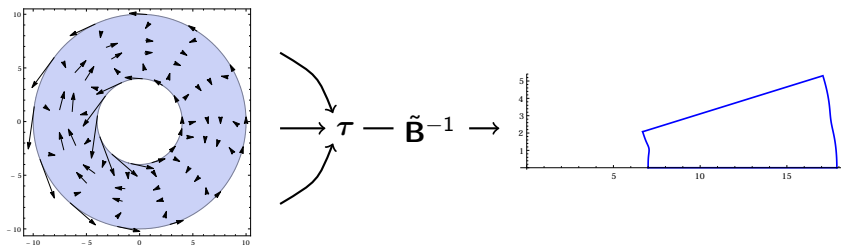
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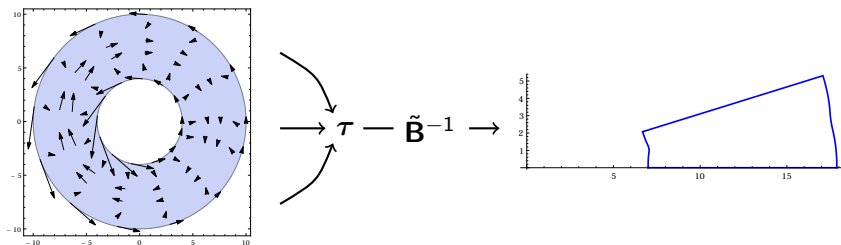


For a given stress field τ

finding a stress-free state embedded in \mathbb{R}^3 is like finding a needle in a nine dimensional haystack.

Stress τ as Input

Looking for a "cut" stress-free state:



For a given stress field τ

finding a stress-free state embedded in \mathbb{R}^3 is like finding a needle in a nine dimensional haystack.

- Is it necessary that the vitural state be an embedding in \mathbb{R}^3 ?

Where to now?

- This method takes a measured τ and produces $W(\mathbf{C}, \tau)$.

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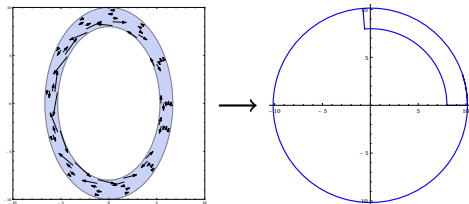
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Any questions?



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Any questions?

Thanks for listening and hope you enjoyed the talk!

-  M. Shams and M. Destrade and R.W. Ogden, Initial stresses in elastic solids: Constitutive laws and acoustoelasticity, Wave Motion, 48 (2011) 552 – 567.
-  Jose Merodio, Ray W. Ogden, Javier Rodriguez, The influence of residual stress on finite deformation elastic response, International Journal of Non-Linear Mechanics, 56 (2013), 43 – 49.